

Optimized Electrical and Thermal Layout of 1700V 450A Power Module Through Virtual Prototyping

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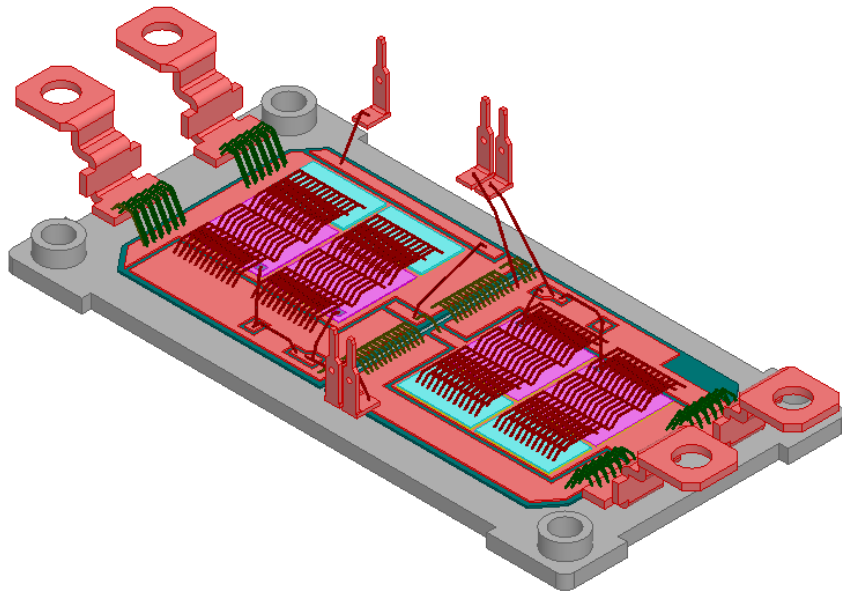
<Nov. 8, 2018>



Outline

- Introduction
- Virtual Prototyping Strategy
 - Methodology
 - Design Evaluation
 - Chips and SPICE Model
- Simulation set-up & Results
 - Thermal Impact
 - Parasitics
 - Switching Behavior
- Experiment & Discussion
 - Impact on Substrate
 - Measurement
- Conclusion

Introduction: The 1700V 450A IGBT Power Module



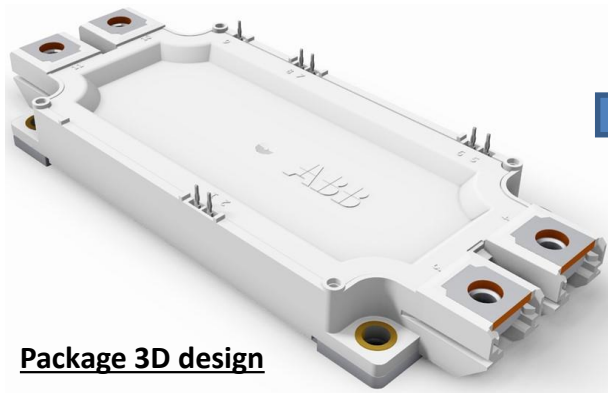
- Evaluate thermal performance
- Include package parasitics in IGBT module performance
- Find balance current distribution
- Find switching currents for power dissipation

Picture: From ABB's Lopak1

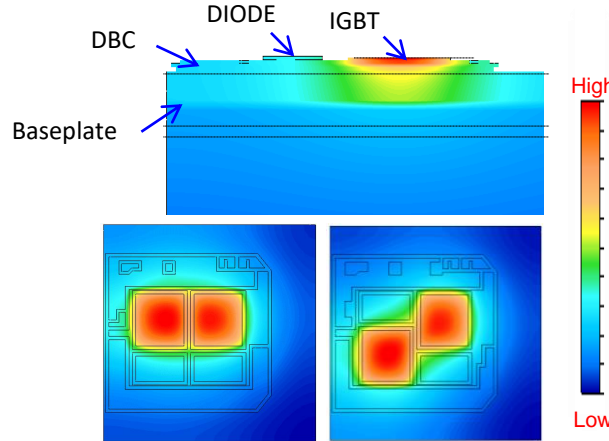
Virtual Prototyping Strategy



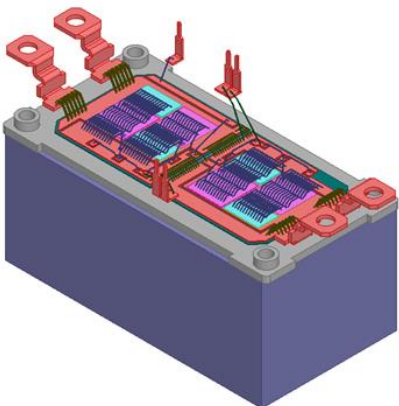
Virtual Prototyping Flow



Thermal Simulation



- 3D concept
- Thermal Simulation
- Package Parasitics
- Electrical Analysis



Simulation: 100MHz [LastAdaptive] [AC RL]

Design Variation:

Profile | Convergence | Matrix | Mesh Statistics

Resistance Units: mOhm Matrix: 100 (MHz) Exp

Inductance Units: nH Original All Freqs

Passivity Tolerance: .0001 Check Passivity Equivalent Circuit Export...

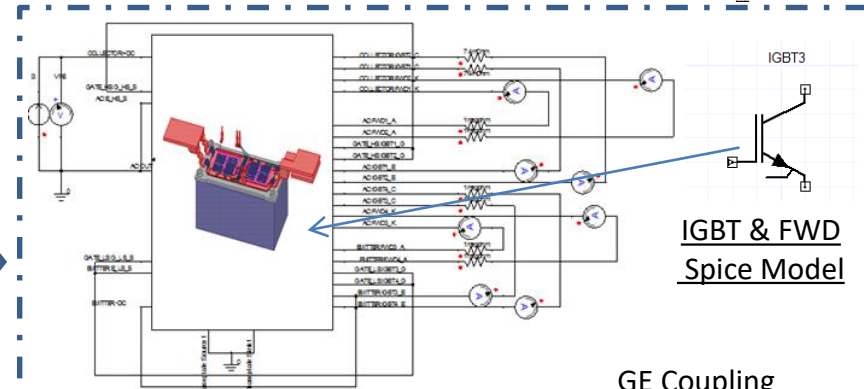
	N1.Source2	P1.Source1
Freq: 100 (MHz)		
N1.Source2	19.63, 16.752	0.4582, 0.94695
P1.Source1	0.4582, 0.94695	6.406, 7.8863

Resistance

$$R = \frac{P}{I_{RMS}^2} = \frac{2P}{I_{peak}^2} \begin{bmatrix} \Delta V_1 \\ \Delta V_2 \end{bmatrix} = \begin{bmatrix} Z_{11} & Z_{12} \\ Z_{12} & Z_{22} \end{bmatrix} \begin{bmatrix} I_1 \\ I_2 \end{bmatrix}$$

Inductance

$$L_{nm} = \int_V \vec{A}_n(\vec{x}) \cdot \vec{J}_n(\vec{x}) dV$$



Electrical Analysis

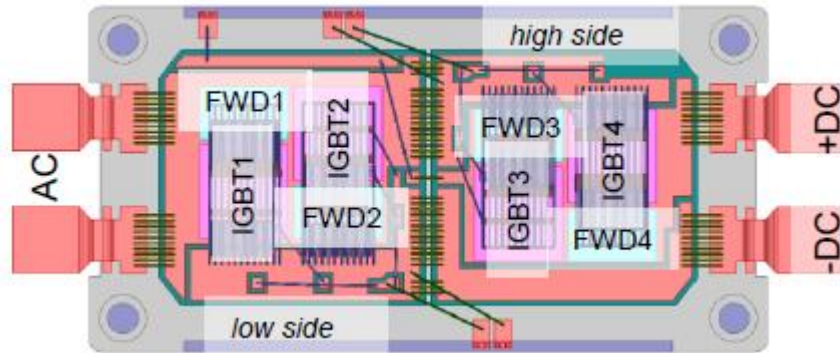
GE Coupling

$$I(t) = \hat{I} \sin(\omega t)$$

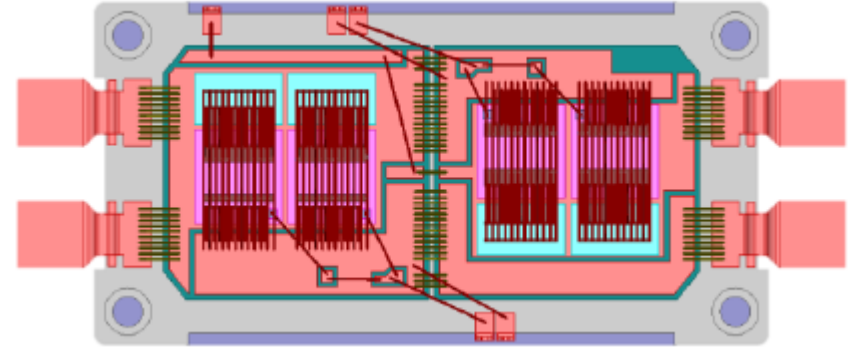
$$V_{GE,x} = R_x \hat{I} \sin(\omega t) + K_x \hat{\omega} \cos(\omega t)$$

Design Evaluation

Concept 1

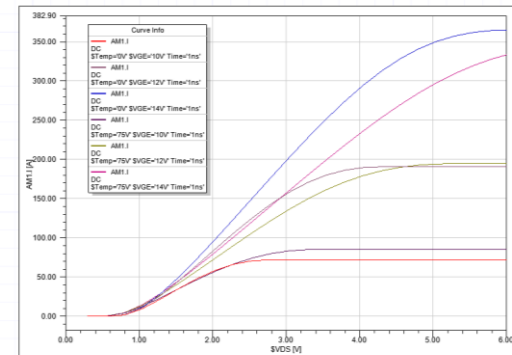
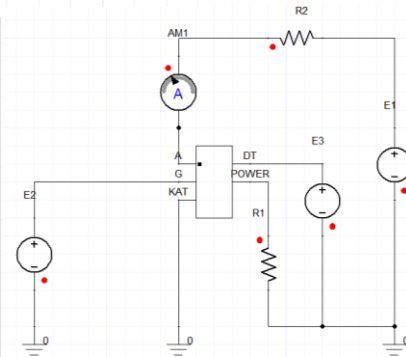
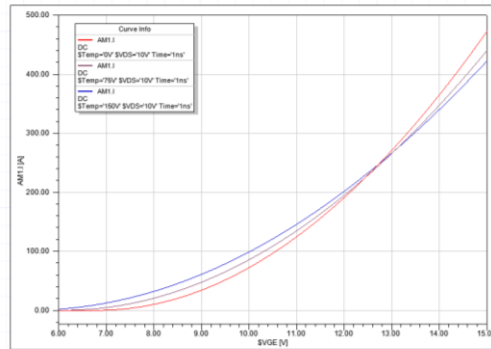
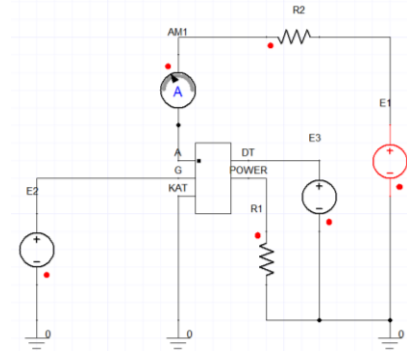
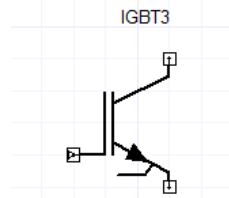


Concept 2



- The LoPak1 module was conceived
 - two possible layout configurations for the IGBTs and FWDs
 - 1st design (concept 1) features an alternating topology of the IGBT and diode
 - 2nd design (concept 2) a parallel topology was implemented

Chips Spice Model



- Compact model was created and tuned to match the die characteristics
- Accurate models of the semiconductors are needed to achieve a good circuit simulation

Simulation set-up & Results

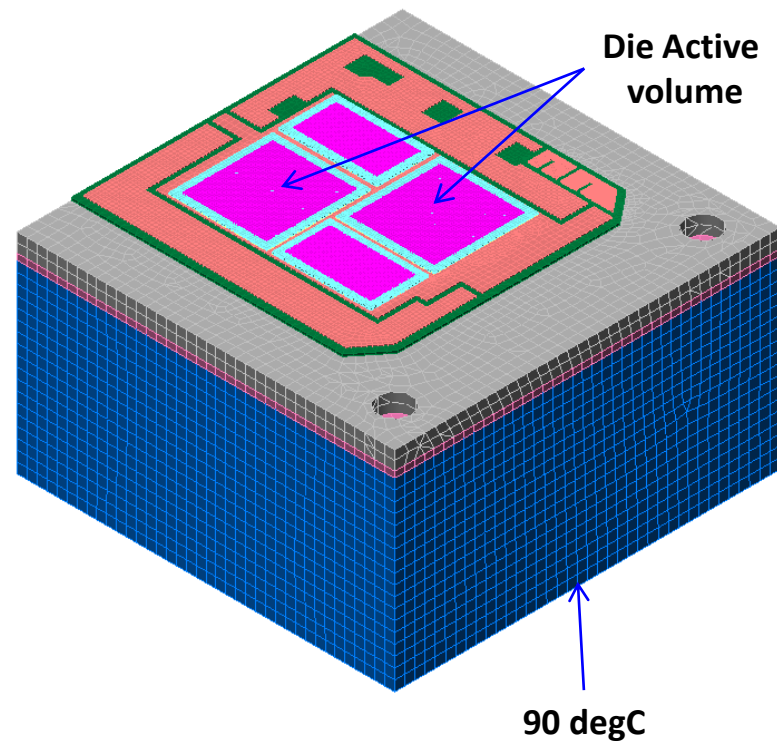


Thermal Impact

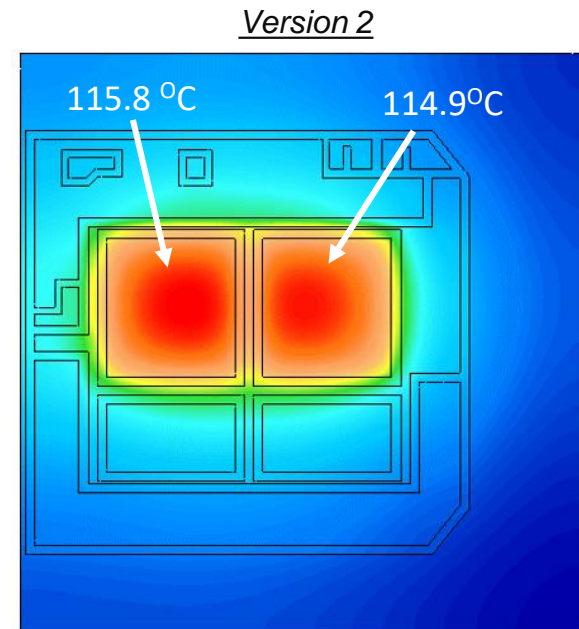
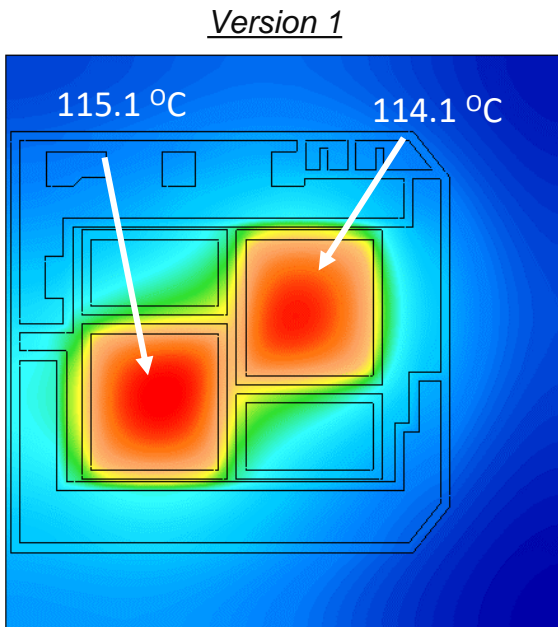
The module layout has to be checked for its thermal distribution & thermal resistance

Materials Mechanical dimension		
Material	Dimension (mm)	Thickness (mm)
IGBT chip	15.9X16.9	0.19
IGBT Active	13.9X14.9	0.060
FWD chip	15.9X9.30	0.390
FWD Active	13.9X7.30	0.130
Chip Solder	-	0.075
Copper Trace	-	0.300
Ceramic	-	0.380
Substrate Solder	-	0.130
Baseplate	-	3.00
TIM	-	0.100
Heatsink	-	30

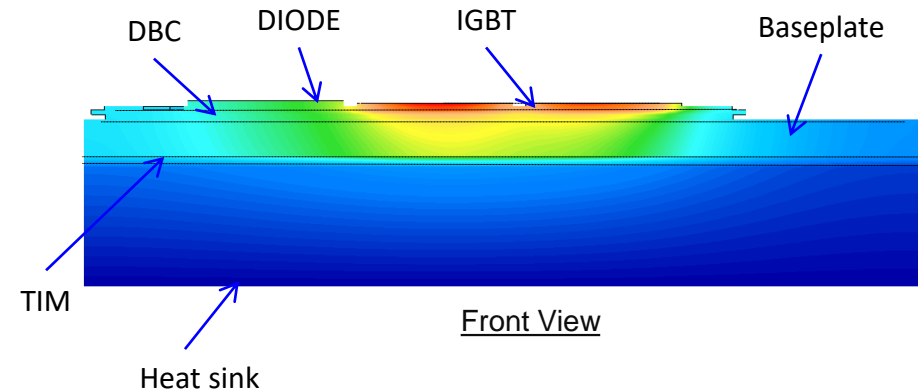
Boundary conditions



Thermal Impact



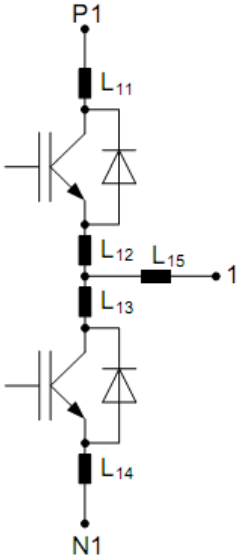
Version 1 supports a little lower junction temp and 3% lower R_{TH}



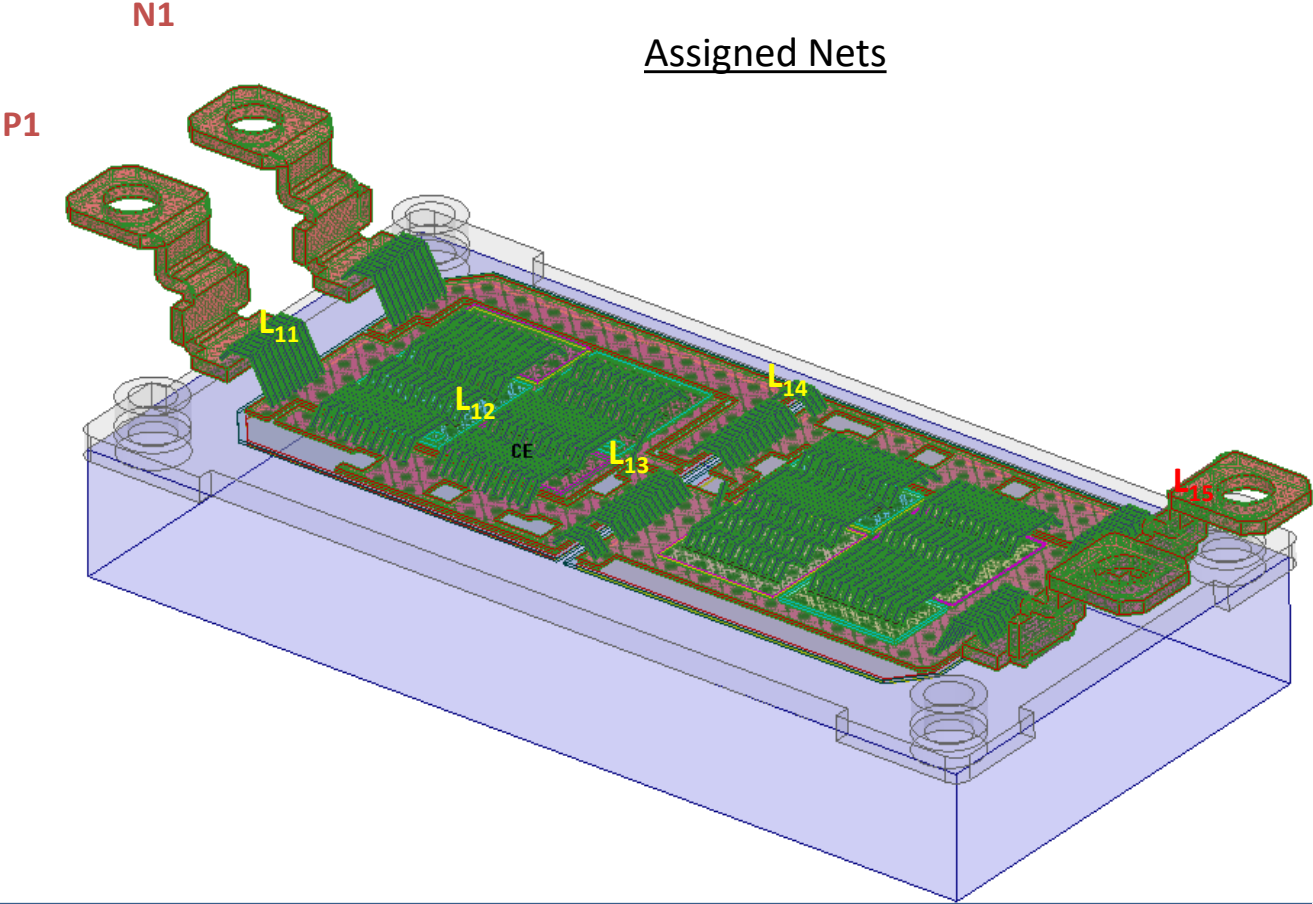
Parasitic Impact

Extracting parameters is straightforward as the nets are automatically assigned

Schematic Diagram



Assigned Nets



Parasitic Impact

Output is composed of RLC matrices at certain frequencies

RL Matrix

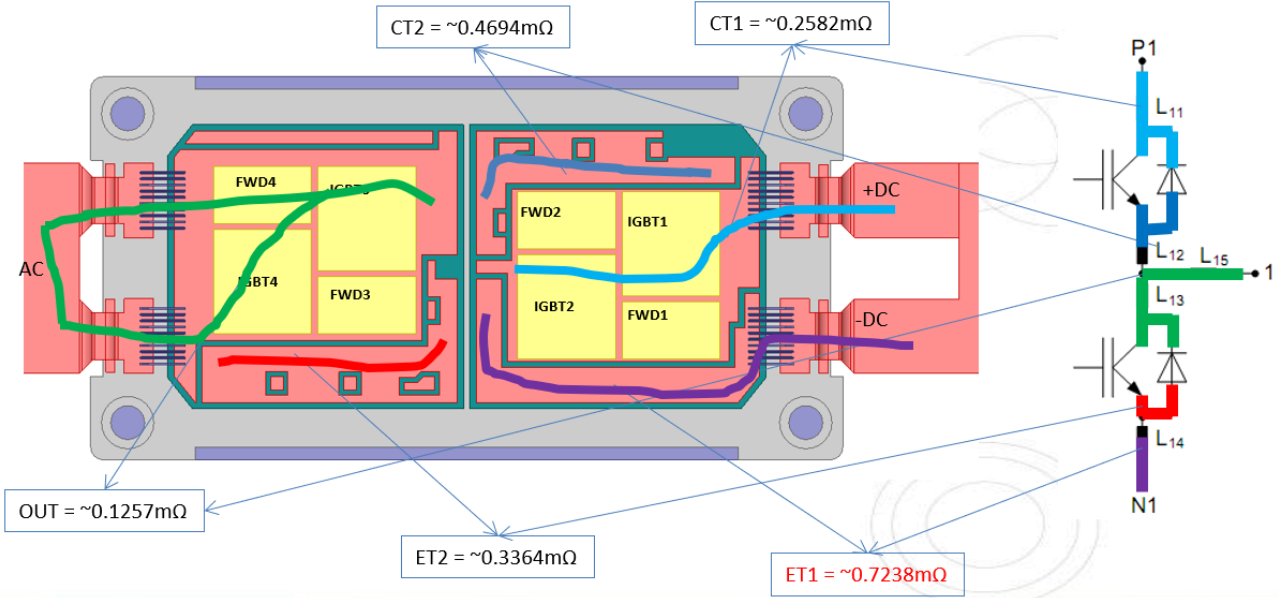
Profile | Convergence | Matrix | Mesh Statistics

Resistance Units: mOhm Matrix 100 (MHz) Exp

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N1:Source2	19.63, 16.752	0.4582, -0.94685
P1:Source1	0.4582, -0.94685	6.406, 7.8863

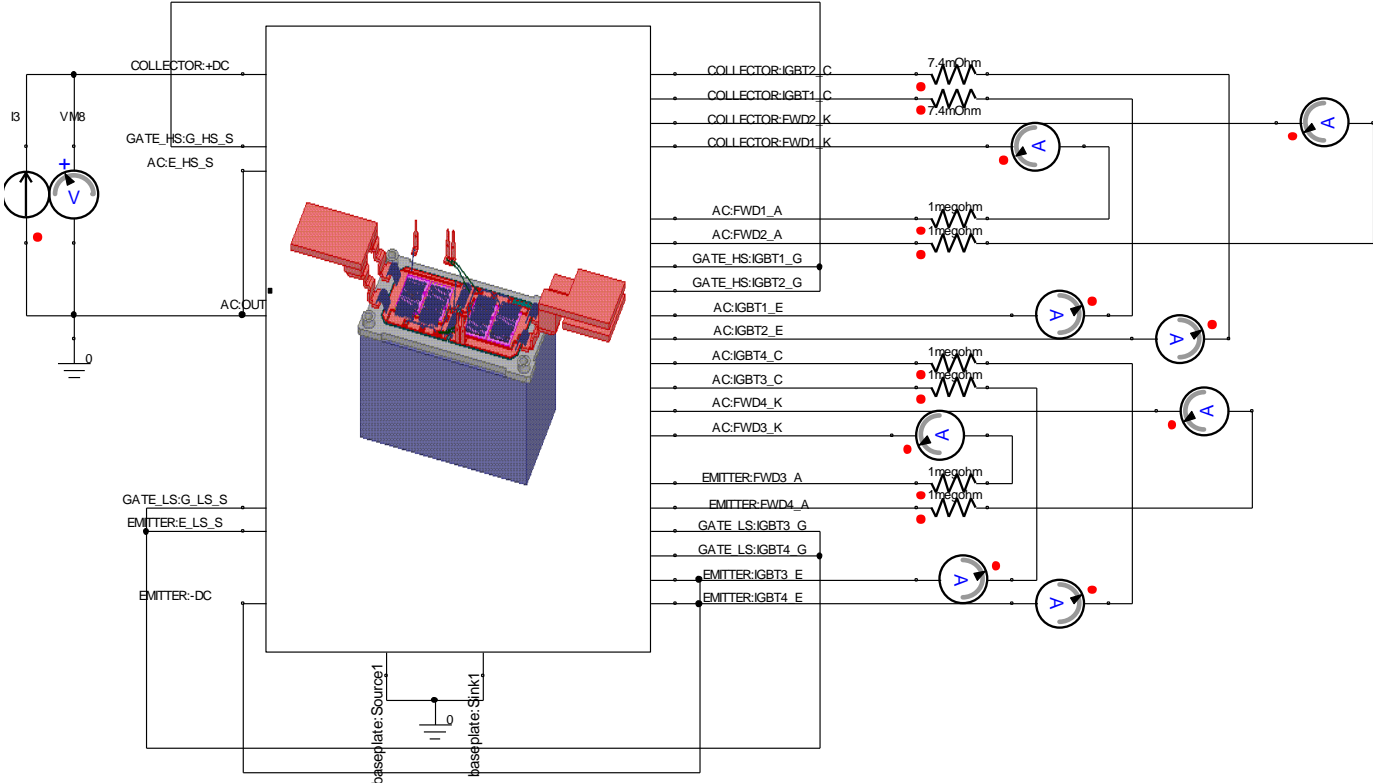


Conducting Nets

- [-] Nets
 - [+] AC
 - [+] baseplate
 - [+] COLLECTOR
 - [+] +DC
 - [+] FWD1_K
 - [+] FWD2_K
 - [+] IGBT1_C
 - [+] IGBT2_C
 - [+] EMITTER
 - [+] -DC
 - [+] E_LS_S
 - [+] FWD3_A
 - [+] FWD4_A
 - [+] IGBT3_E
 - [+] IGBT4_E
 - [+] GATE_HS
 - [+] GATE_LS

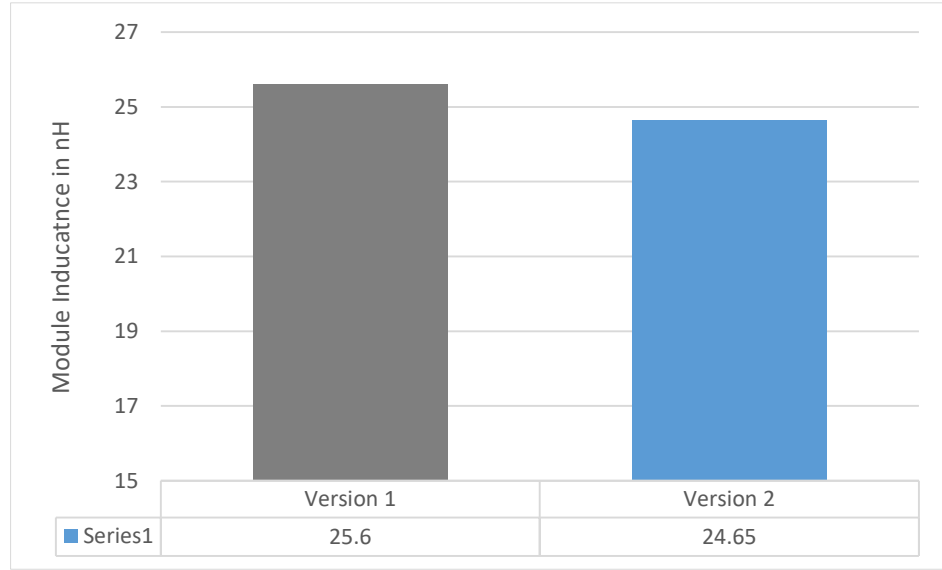
Parasitic - Integration

Using the result of lumped elements [RLC] to SPICE circuit simulator

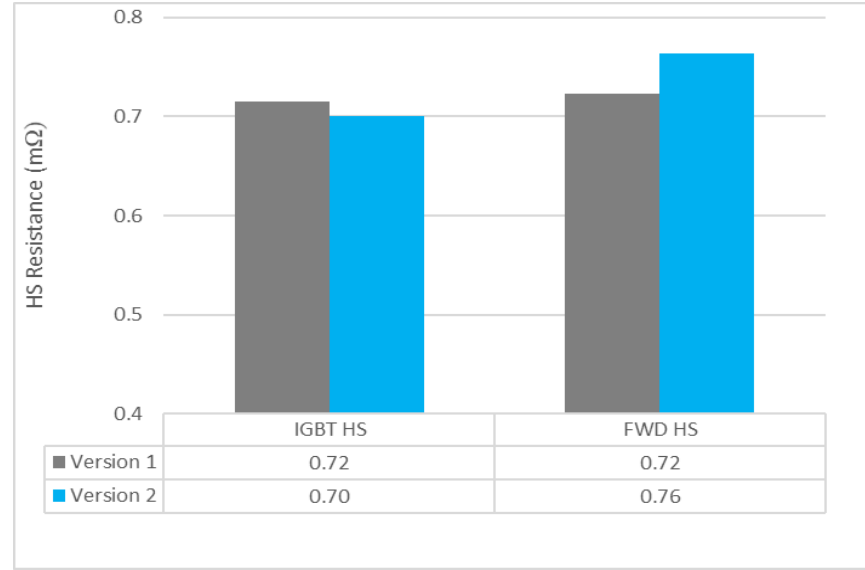


System Simulation – Module Resistance & Inductance

Module Inductance in nH



Module Resistance in mΩ

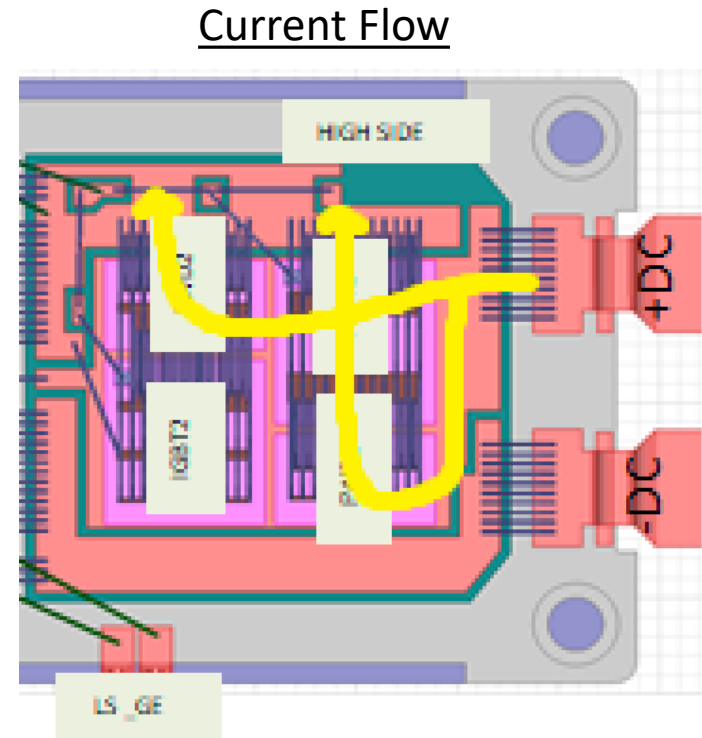
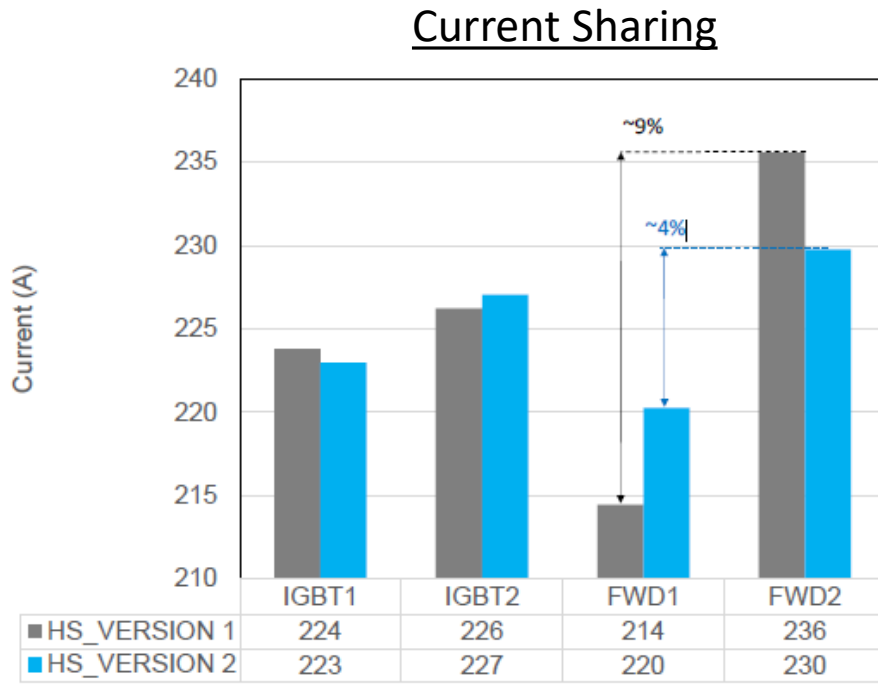


The parasitic extraction confirms:

- Both layout versions do not impact the inductance of the module of about 25nH
- the resistance of around 1mOhm



Parasitic Impact – Current Sharing

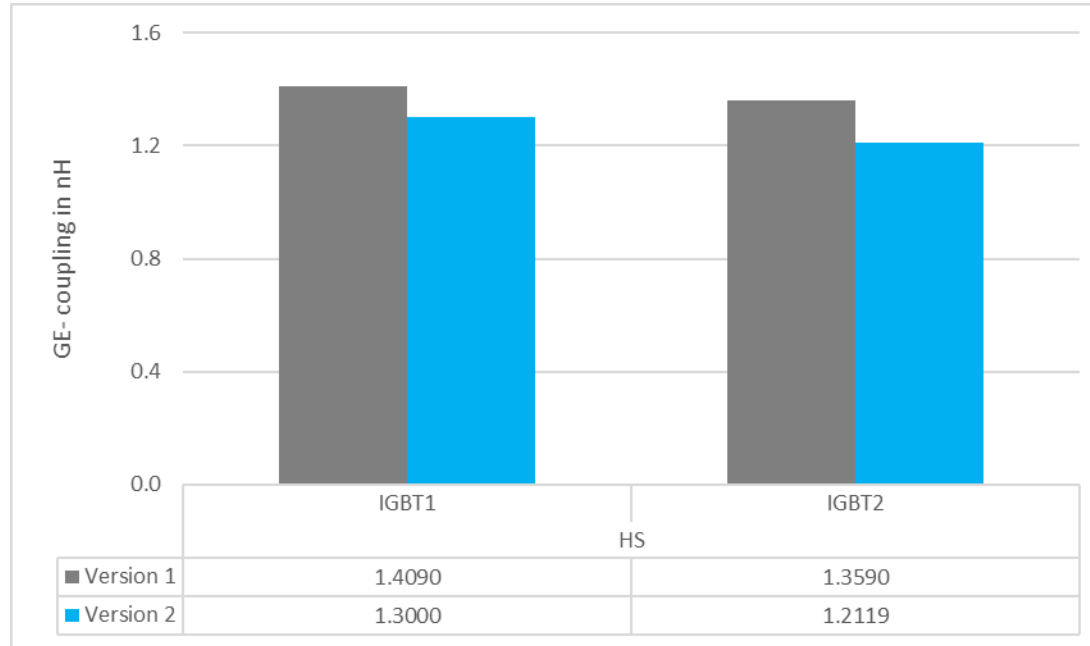


The static current sharing shows significant imbalance:

- For IGBT's are almost equal
- Free-wheeling diodes reaches 22A[version1]
- A similar result in the static current sharing for LS for both version

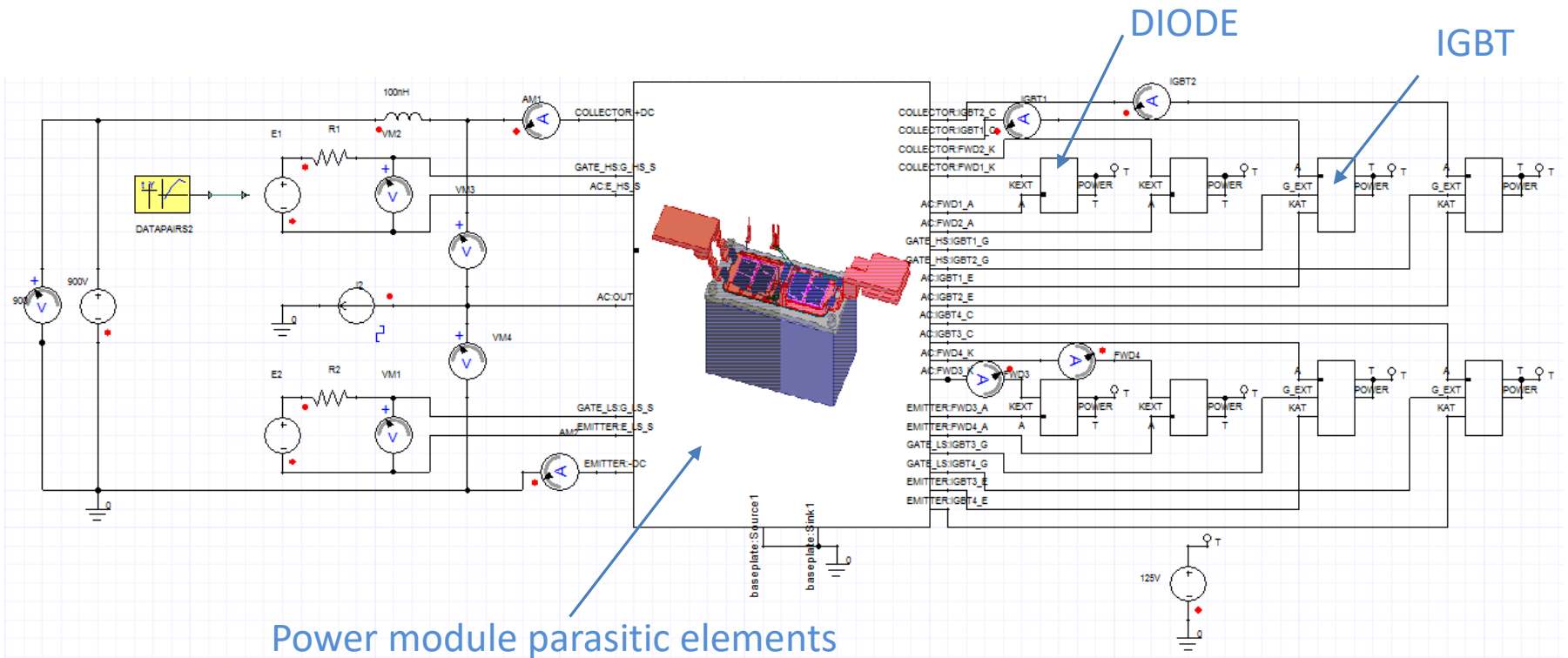
System Simulation – GE Coupling

HS Switch GE Coupling



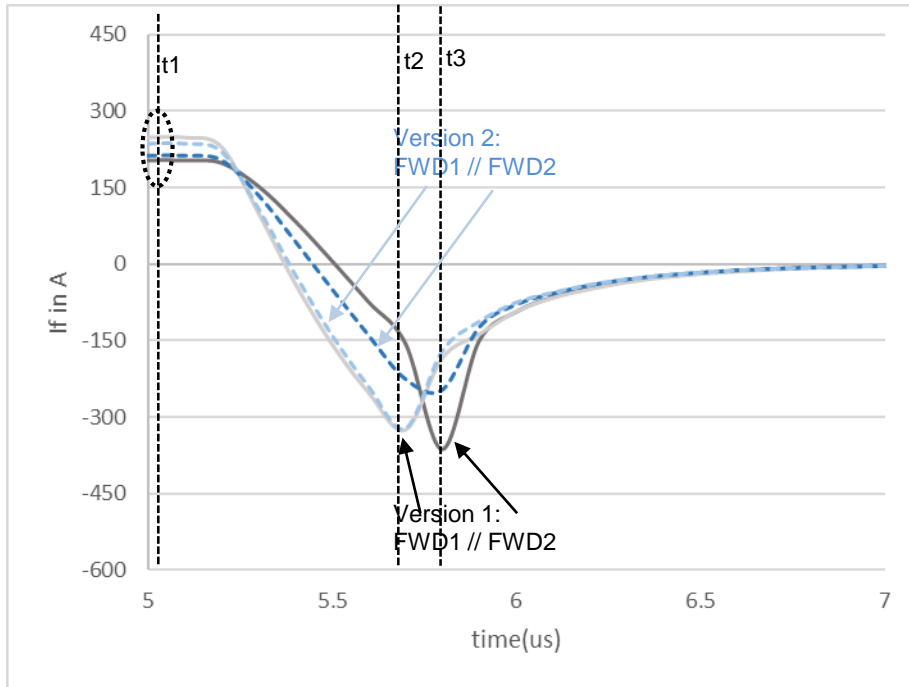
- Gate-emitter coupling of version 2 is lower – affect switching speed

System Simulation

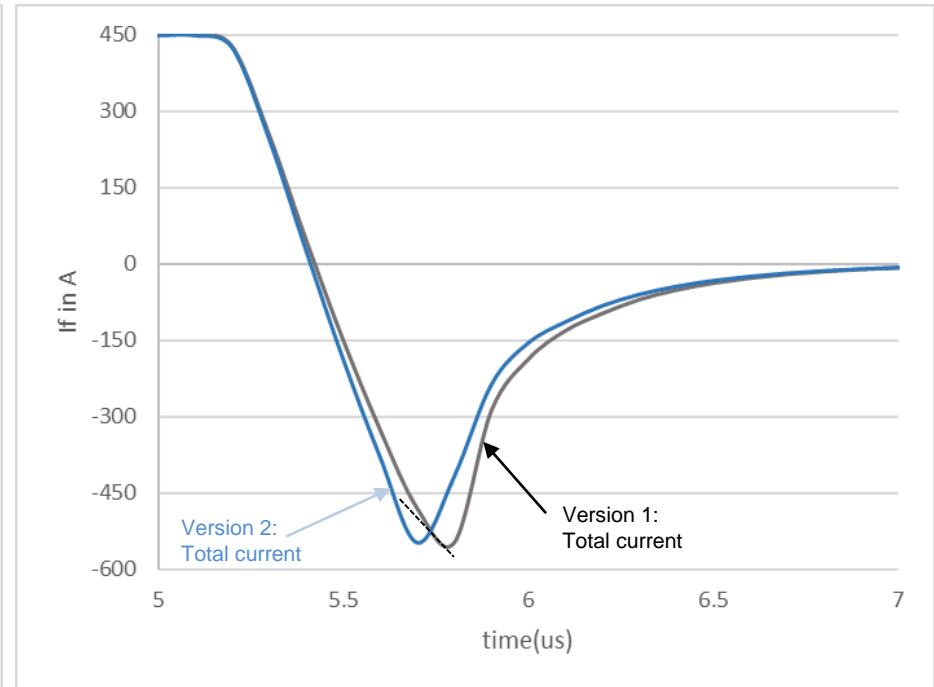


- SPICE models reflecting the chip-properties and the full simulation of a dynamic double-pulse test

System Simulation – Switching



Individual Current Through Diode



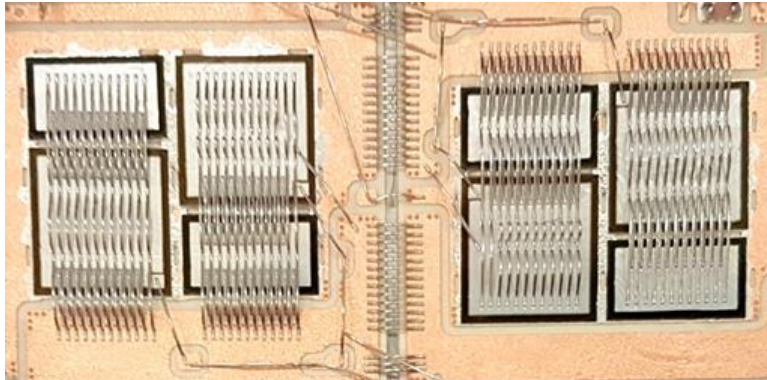
Total Current – Sum of FWD 1&2 Both Versions

Experiment & Discussion

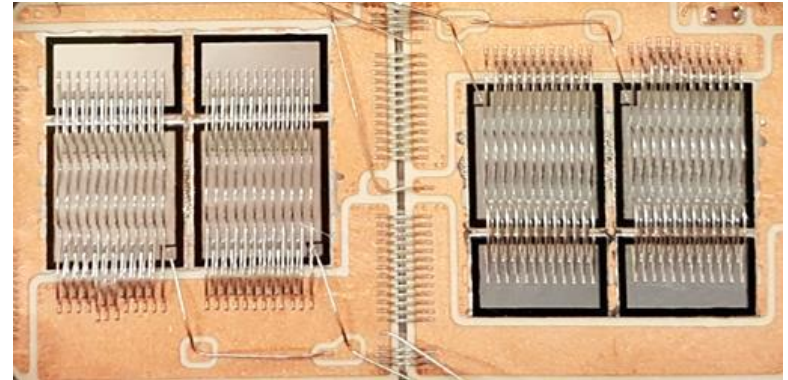


Impact on Substrate Layout

Version 1 - Actual



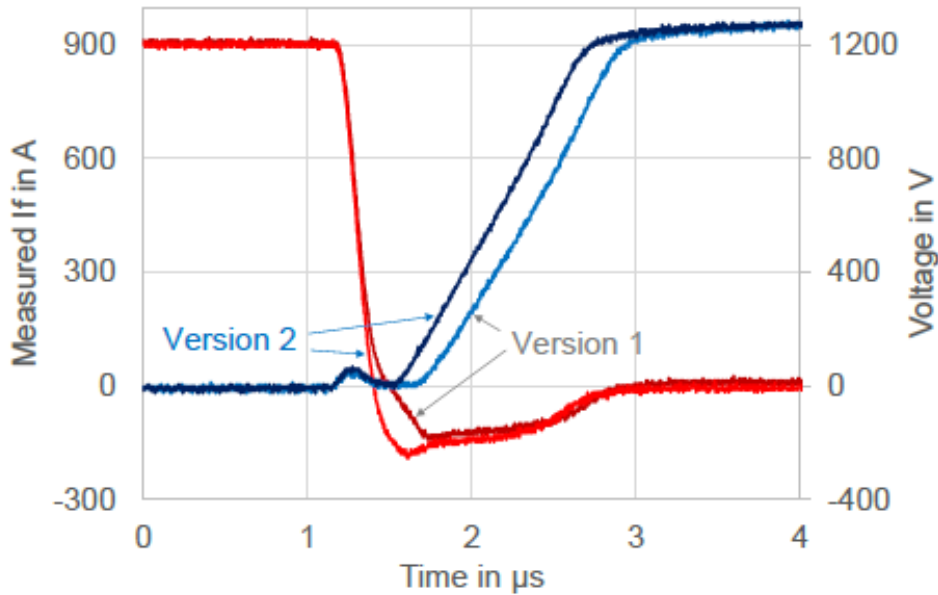
Version 2 - Actual



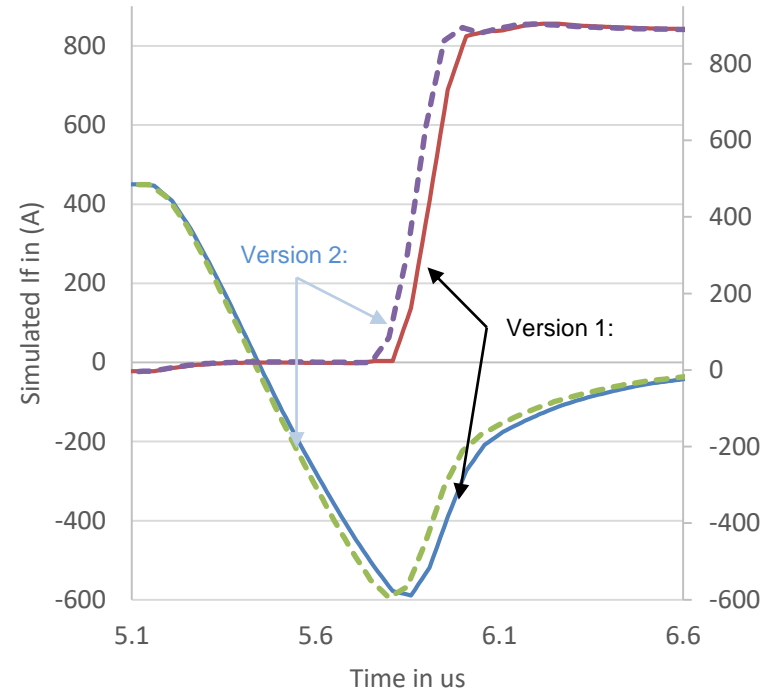
- Both layout versions were fabricated
- The electrical properties were characterized
 - Static & standard double pulse
 - Focus is on diode turn-off behavior

Electrical Measurement

Actual Testing



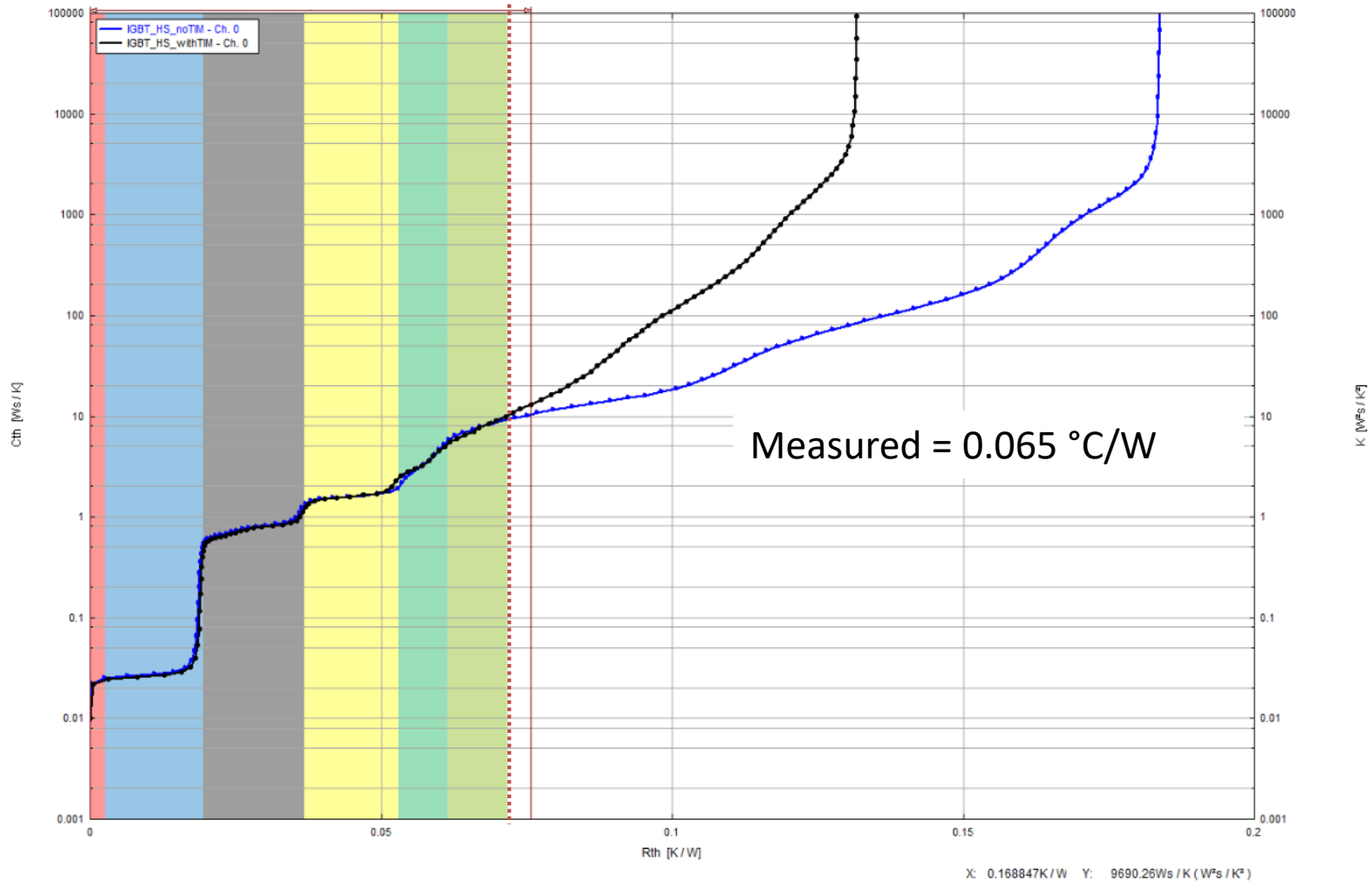
Simulated



Experimental results of the diode turn-off for the high-side switch – comparison of version 1 and 2 for safe-operating area conditions: $V_{dc}=1300V$, $I_c=900A$ ($2 \times I_{nominal}$), $T_j=25^\circ C$, $V_{ge}=15V$, $R_g=0.2 \text{ Ohm}$).

Thermal Measurement

R_{TH} (junction to case) – IGBT [Version 2]



Conclusions



Conclusions

- Complete virtual prototyping approach
 - Concept with accurate 3D concept and geometry
 - Thermal sizing through FEM simulation
 - Parasitic extraction to perform co-simulation
 - Complete dynamic simulation
- Layout optimization
 - Designed for equilibrated current sharing
 - Temperature distribution
 - Switching behavior

Conclusions

- Actual testing
 - Confirmed the predictive power of simulations
 - Certain crucial features in the current and voltage waveforms were predicted and could be experimentally reproduced during the characterization
- Business Benefits
 - Communication is more effective, errors reduced, and more innovative product designs are delivered faster
 - Reduce cost of development and shorten time to market

Acknowledgement

- ABB & IMI

Optimized layout of 1700V LoPak1 IGBT power module by holistic design approach

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